

Numerical modelling of the dynamic behaviour of masonry constructions



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- The NOSA code is a finite element solver for nonlinear analyses.
- Masonry is modelled by a nonlinear isotropic elastic material with zero tensile strength and limited compressive strength (masonry-like or no-tension material). [G. Del Piero, *Meccanica* 1989; S. Di Pasquale, *Meccanica* 1992; M. Lucchesi, C. Padovani et al., *Masonry Constructions and Numerical Applications*, Springer 2008].

- Static analyses
- Dynamic analyses
- Thermo-mechanical analyses



- Stress fields
- Collapse loads
- Elastic, fracture and crushing strain fields
- Displacement fields
- Temperature fields
- Time- histories

- NOSA library: beam, shell, 2D, 3D elements (17 elements)

The NOSA version for static analyses is freely downloadable by
www.isti.cnr.it/research/unit.php?unit=MMS§ion=software

The masonry-like constitutive equation

- \mathbf{E} the infinitesimal strain tensor,
- \mathbf{T} the Cauchy stress tensor,
- \mathbf{E}^e the elastic part of the strain,
- \mathbf{E}^f the fracture strain,
- \mathbf{E}^c the crushing strain,
- \mathbf{E}, ν the modulus of elasticity and the Poisson's ratio,
- $\sigma_0 < 0$ the masonry maximum compressive stress.

Given \mathbf{E} , find \mathbf{E}^f , \mathbf{E}^c , \mathbf{T} such that

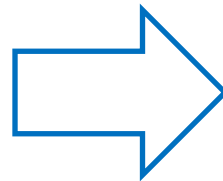
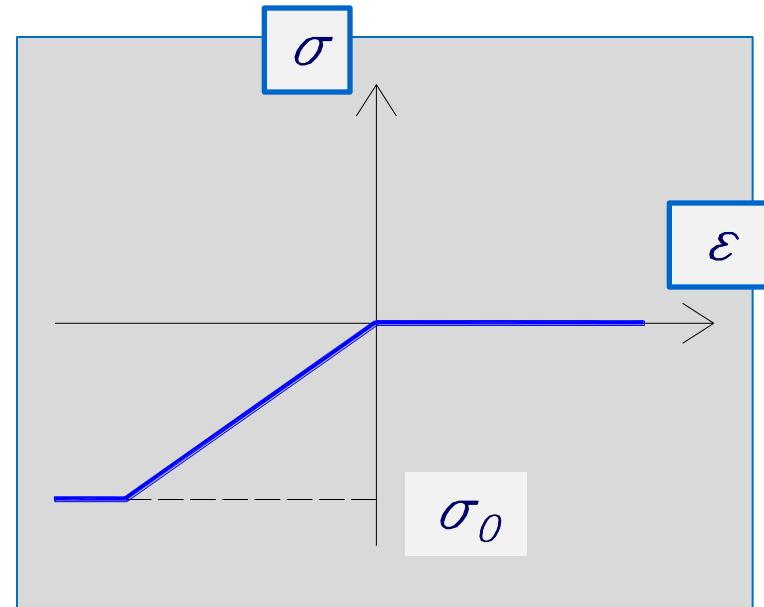
$$\mathbf{E} = \mathbf{E}^e + \mathbf{E}^f + \mathbf{E}^c,$$

$$\mathbf{E}^f \cdot \mathbf{E}^c = \mathbf{0},$$

$$\mathbf{T} = \frac{\mathbf{E}}{1+\nu} \left[\mathbf{E}^e + \frac{\nu}{1-2\nu} \text{tr}(\mathbf{E}^e) \mathbf{I} \right],$$

$$\mathbf{T} \cdot \mathbf{E}^f = (\mathbf{T} - \sigma_0 \mathbf{I}) \cdot \mathbf{E}^c = \mathbf{0},$$

$$\mathbf{T}, \mathbf{E}^c \leq \mathbf{0}, \quad \mathbf{T} - \sigma_0 \mathbf{I} \geq \mathbf{0}, \quad \mathbf{E}^f \geq \mathbf{0}$$



$$\mathbf{T} = \hat{\mathbf{T}}(\mathbf{E}), \quad \mathbf{D}_{\mathbf{E}} \hat{\mathbf{T}}(\mathbf{E})$$

Some example applications

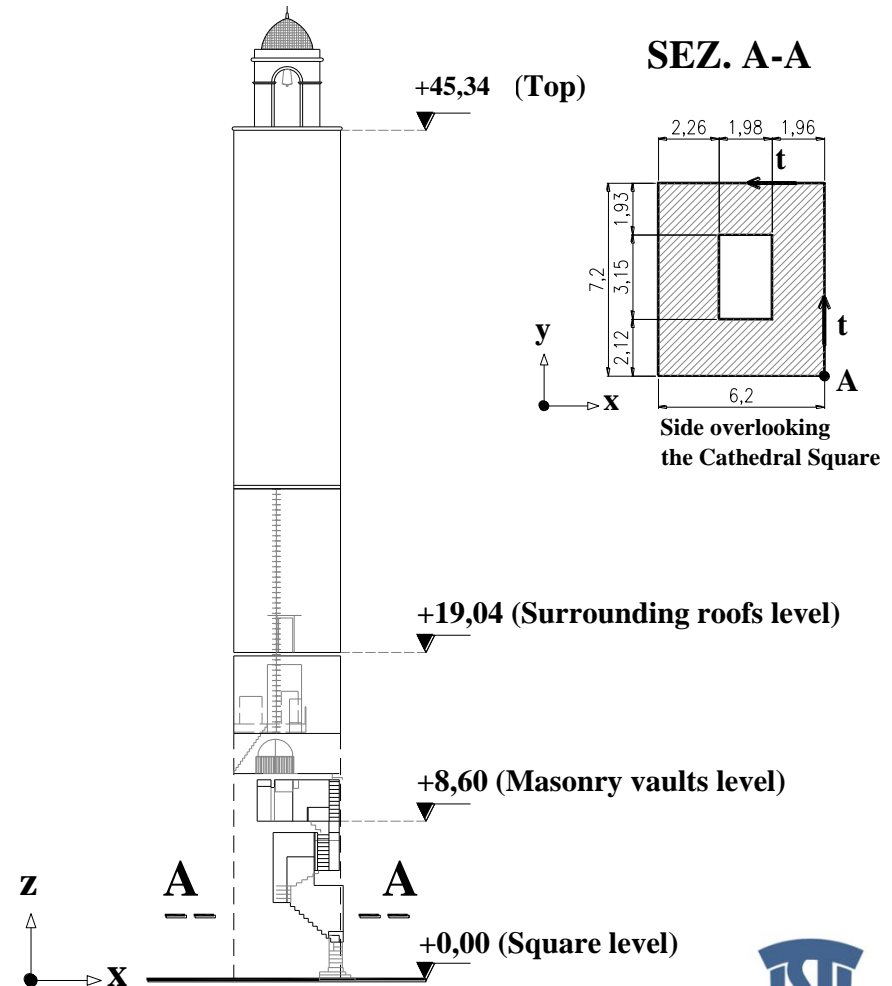
Static Analyses

- 1995 Battistero del Duomo, Volterra
- 1996 Arsenale Mediceo, Pisa
- 1998 Teatro Goldoni, Livorno
- 1998 Chiesa Madre di S. Nicolò, Noto
- 2004 Chiesa di Santa Maria Maddalena, Morano Calabro
- 2005 Chiesa di San Ponziano, Lucca

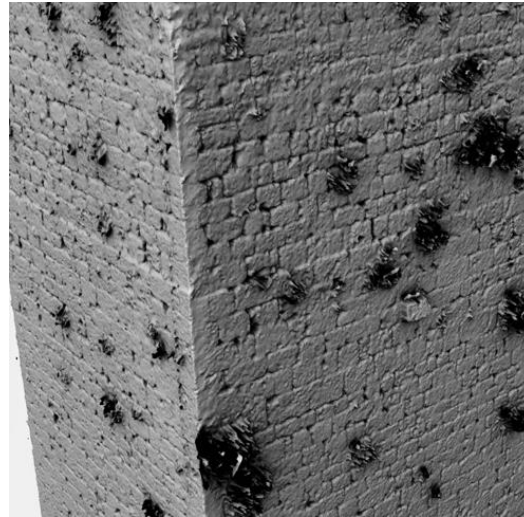
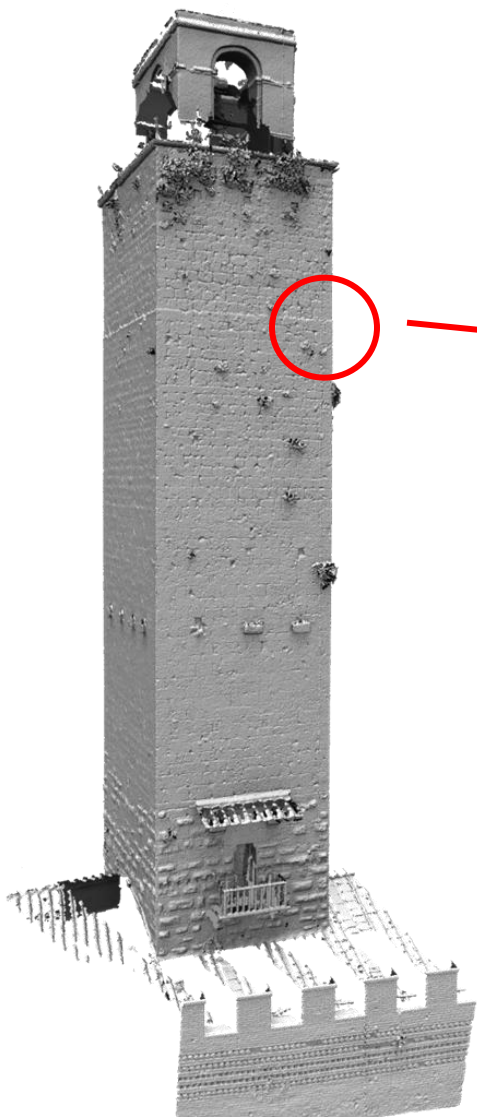
Dynamic Analyses

- 2008 Chiesa Abbaziale di Santa Maria della Roccella, Roccella Ionica
- 2008 Torre "Rognosa" , San Gimignano
- 2010 Torre "delle Ore", Lucca

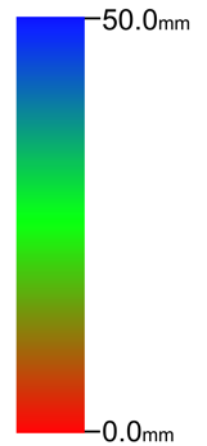
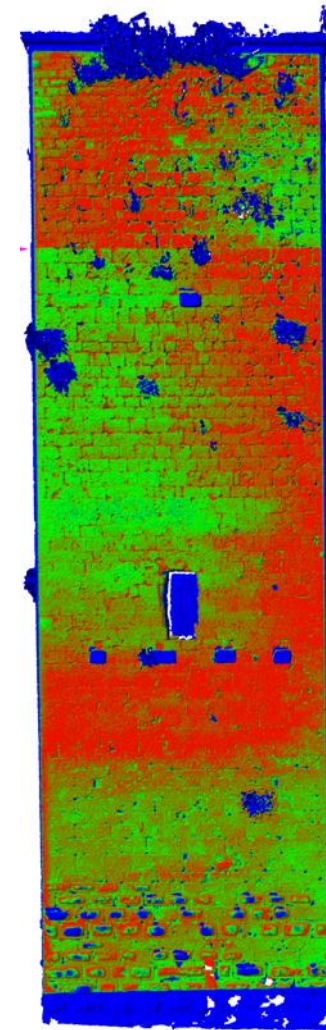
The "Rognosa" tower in San Gimignano (St@rt project)



The "Rognosa" tower in San Gimignano: digital acquisition of the geometry
(VC Lab – ISTI CNR)

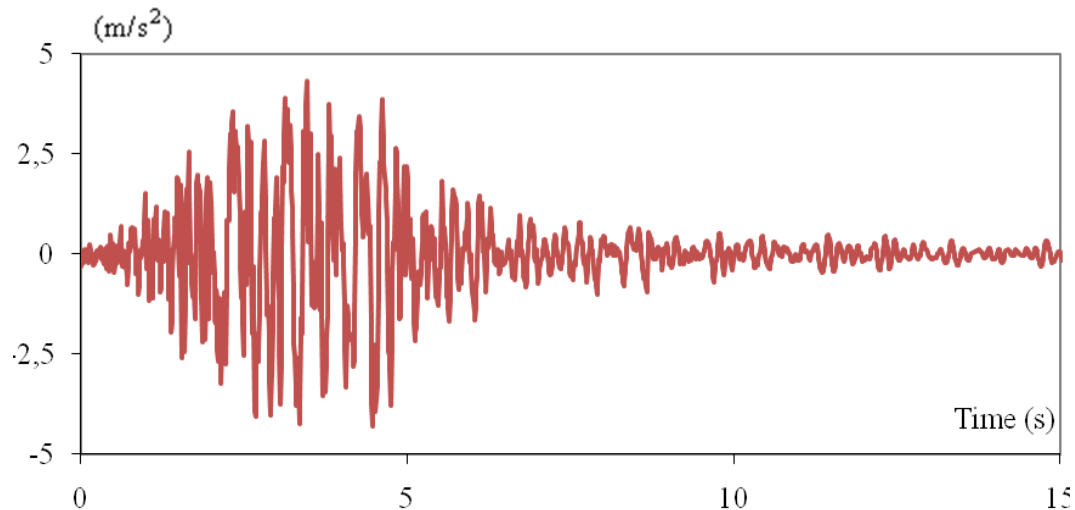


Merging resolution=1 cm



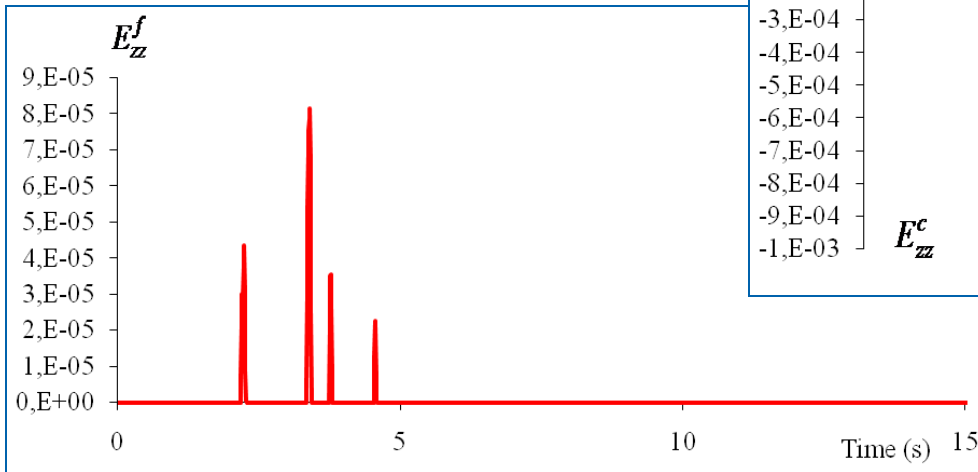
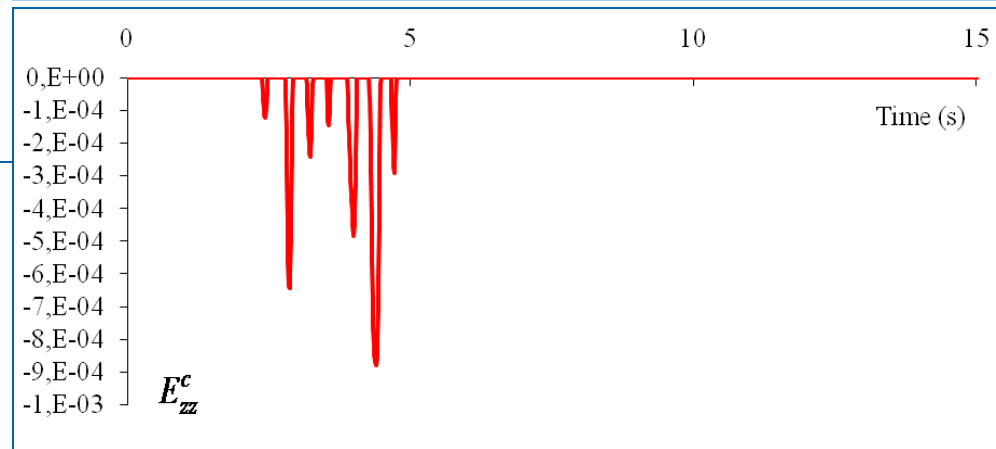
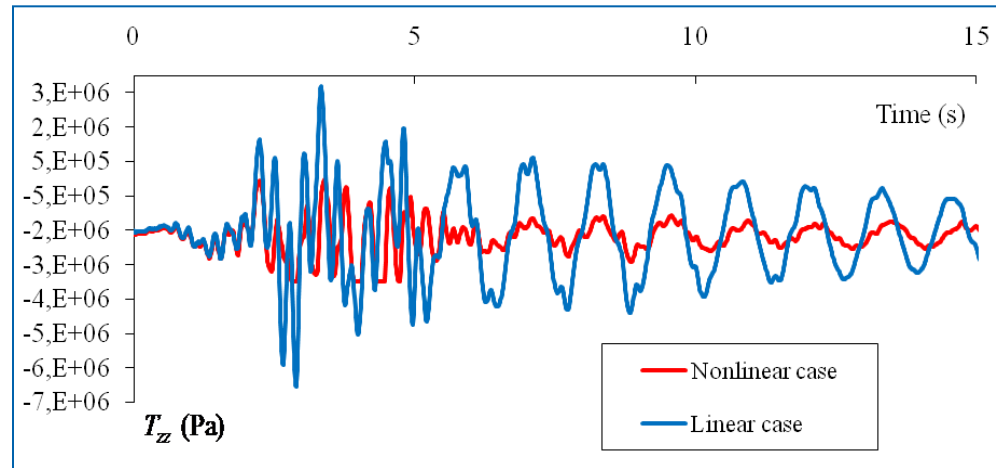
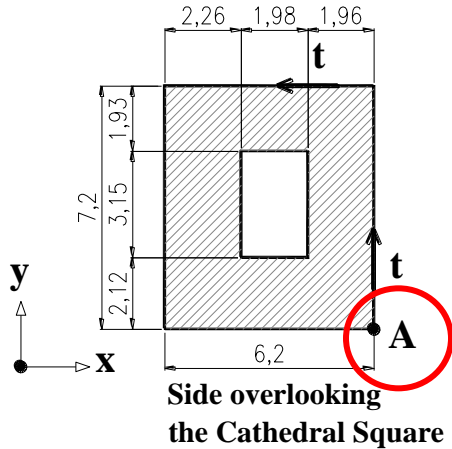
The "Rognosa" tower in San Gimignano:

- **Static analysis** The Tower is subjected to its own weight and to the weight of the surrounding buildings
- **Dynamic analysis** The Tower subjected to the Nocera Umbra earthquake in x - direction

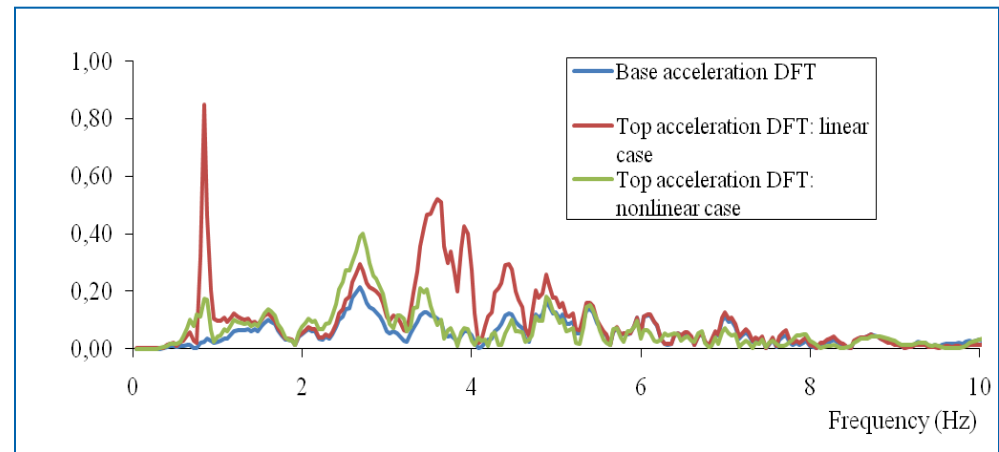
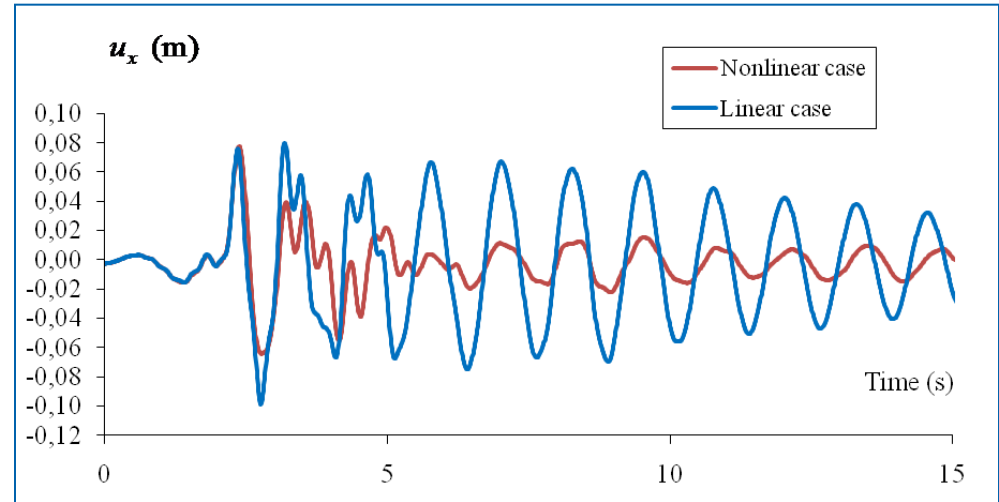
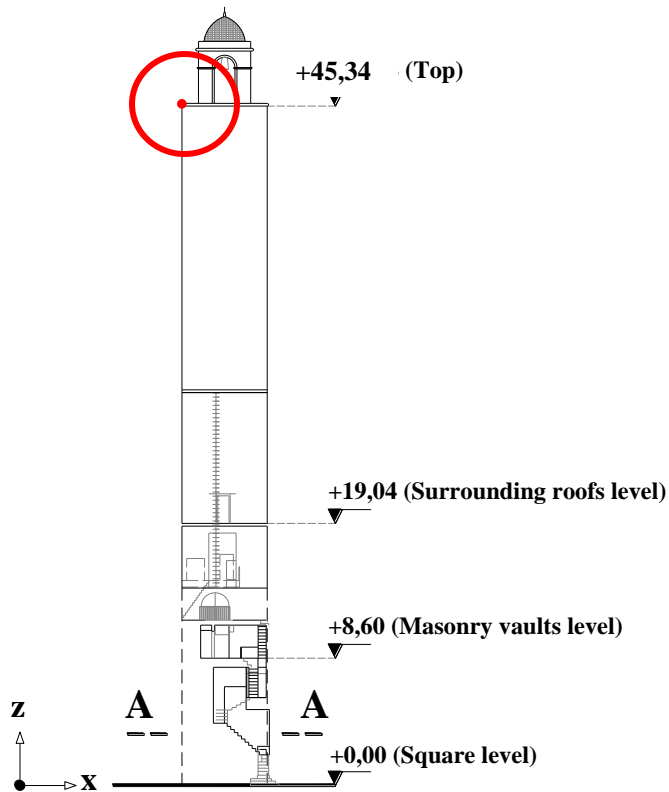


The "Rognosa" tower in San Gimignano: dynamic analysis

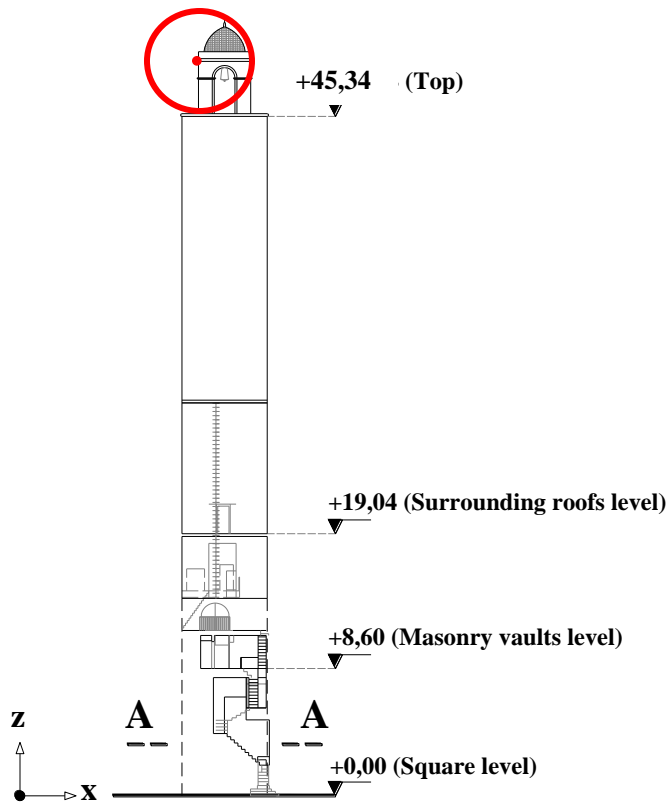
Tower base section



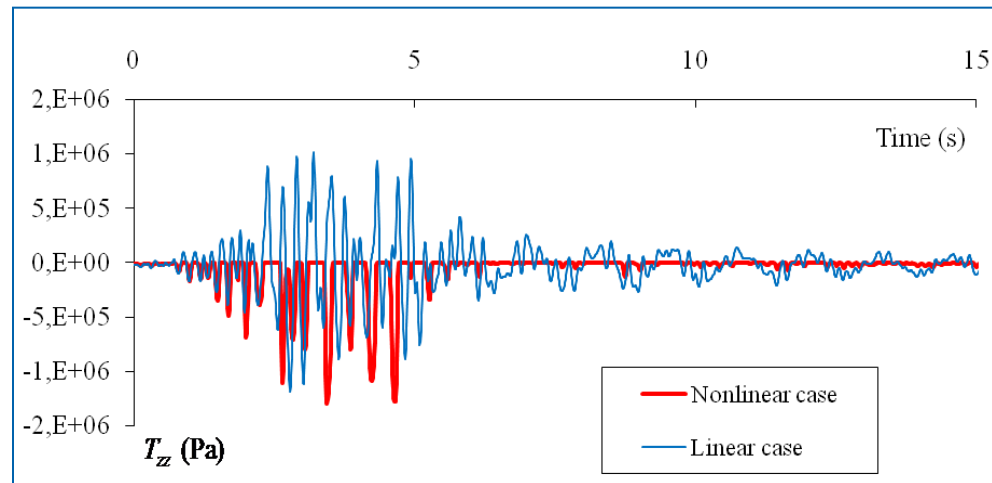
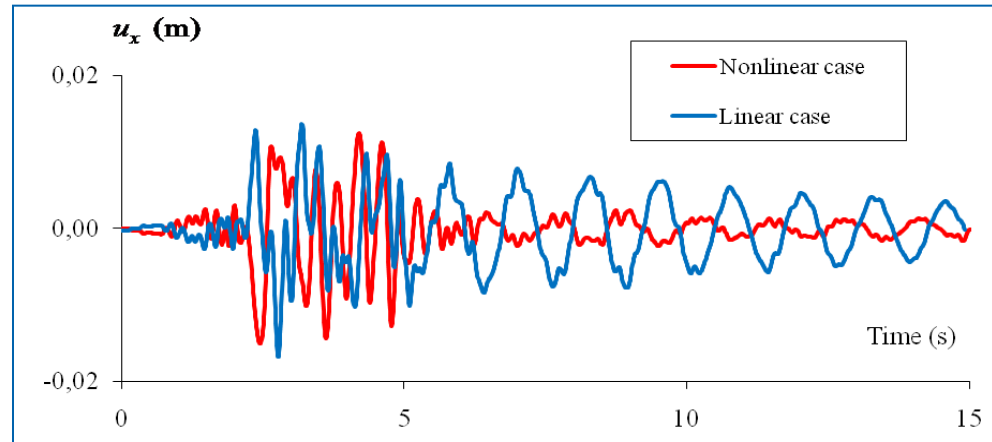
The "Rognosa" tower in San Gimignano: dynamic analysis



Tower vertical section



The bell chamber

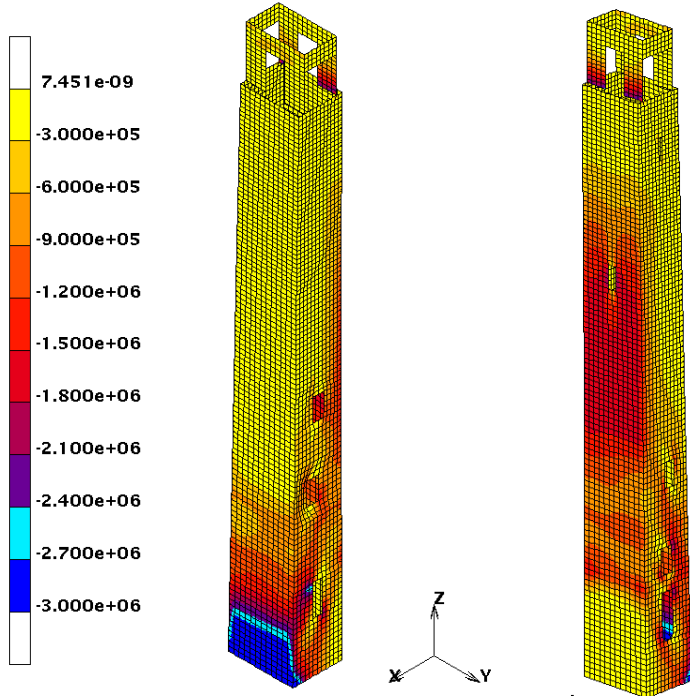


The "Rognosa" tower in San Gimignano: dynamic analysis

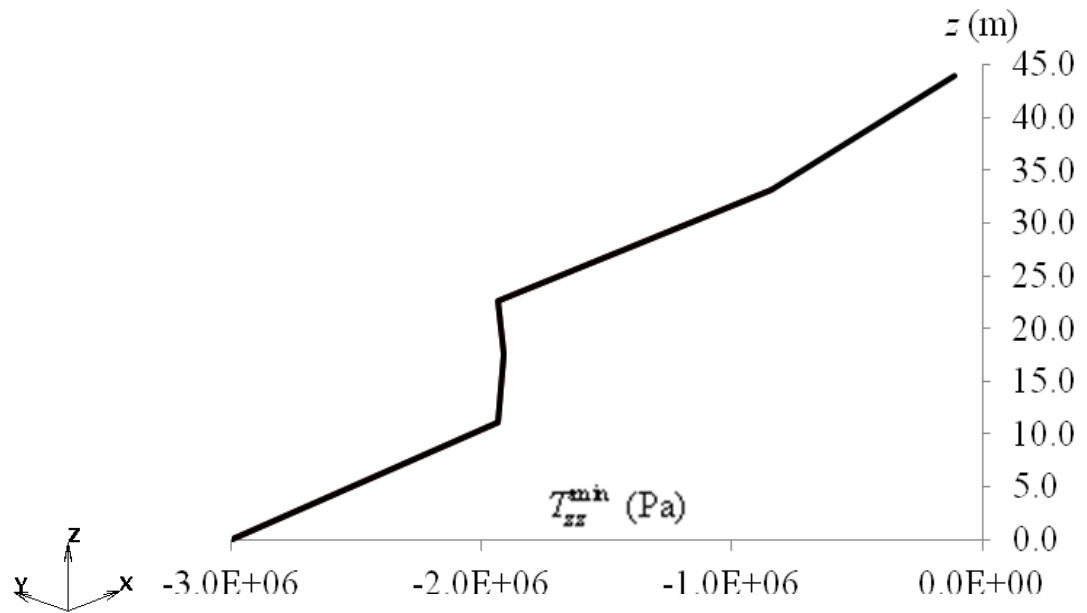
Compressive stresses T_{zz}

At time $t=3,41$ s:

Inc: 343
Time: 3.410e+00



Minimum values reached during the analysis :

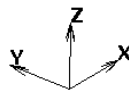
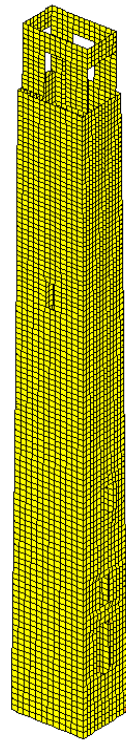
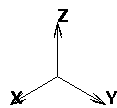
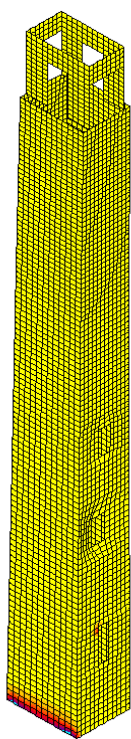
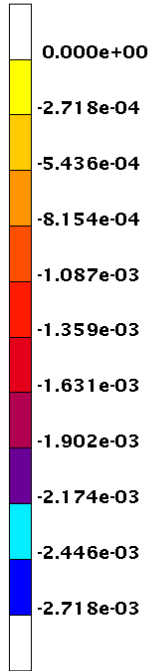


The "Rognosa" tower in San Gimignano: dynamic analysis

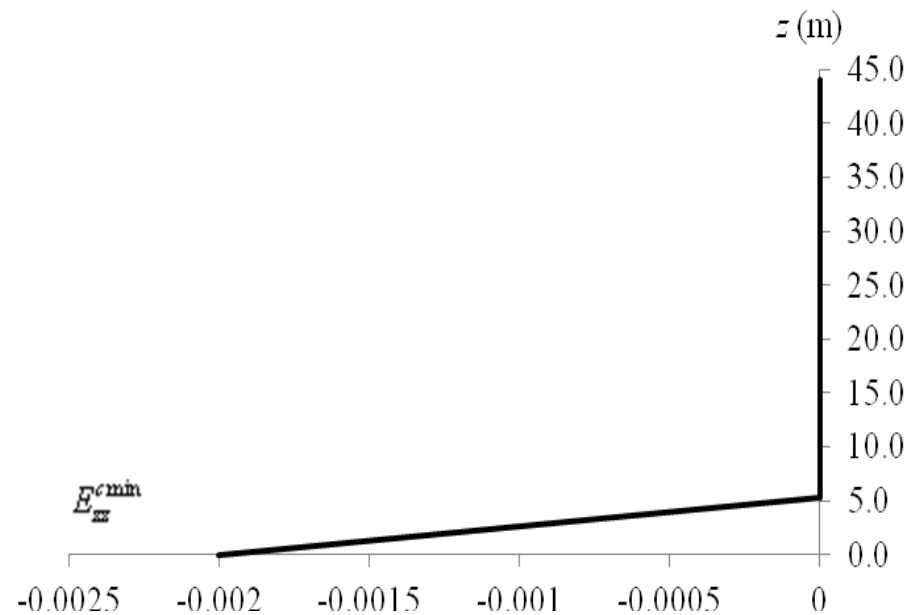
Crushing strain E_{zz}^c

At time $t=3,41$ s:

Inc: 343
Time: 3.410e-



Minimum values reached during the analysis :

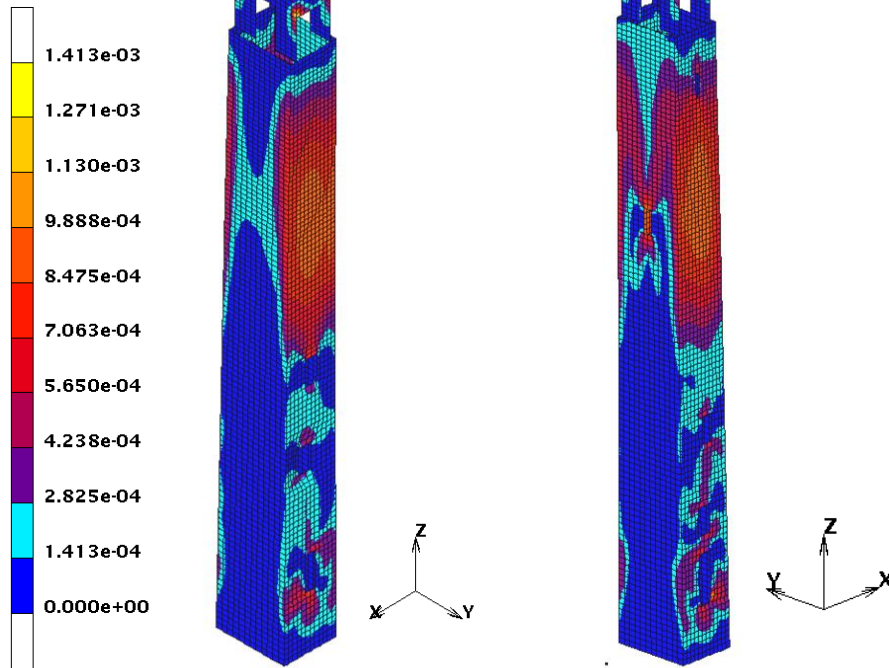


The "Rognosa" tower in San Gimignano: dynamic analysis

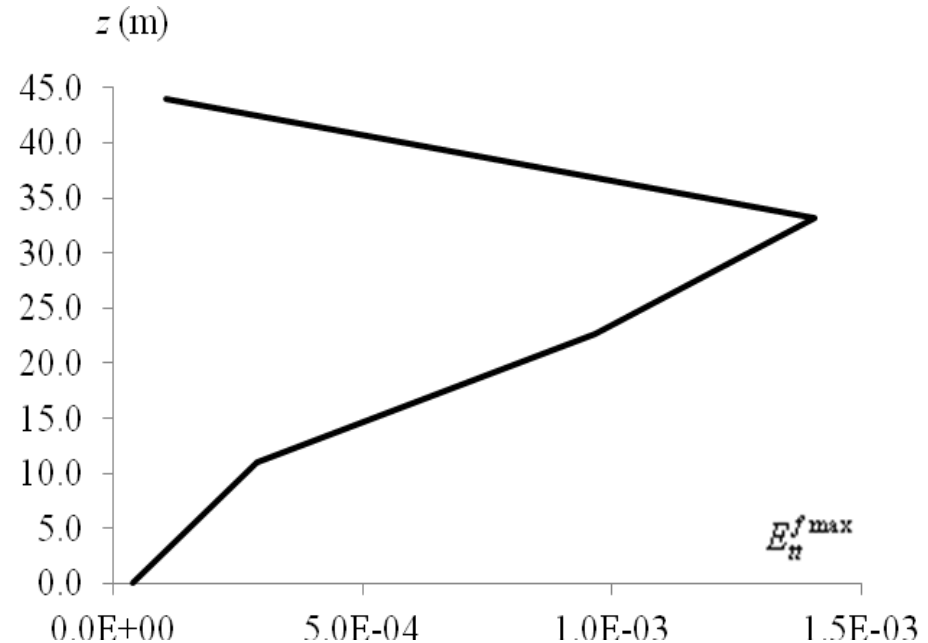
Tangential fracture strain E_{tt}^f

At time $t=3,41$ s:

Inc: 343
Time: 3.410e+



Maximum values reached during the analysis :

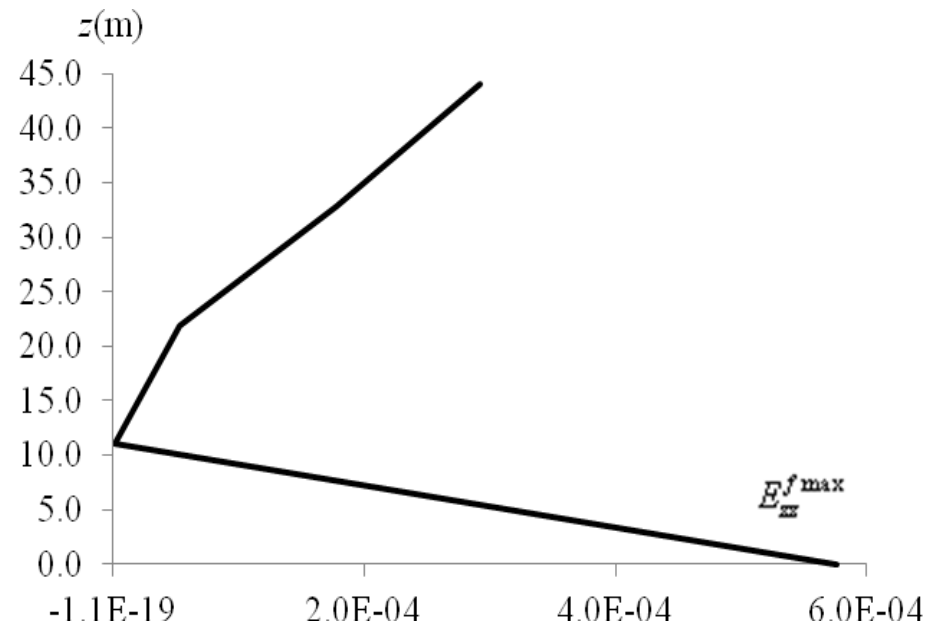
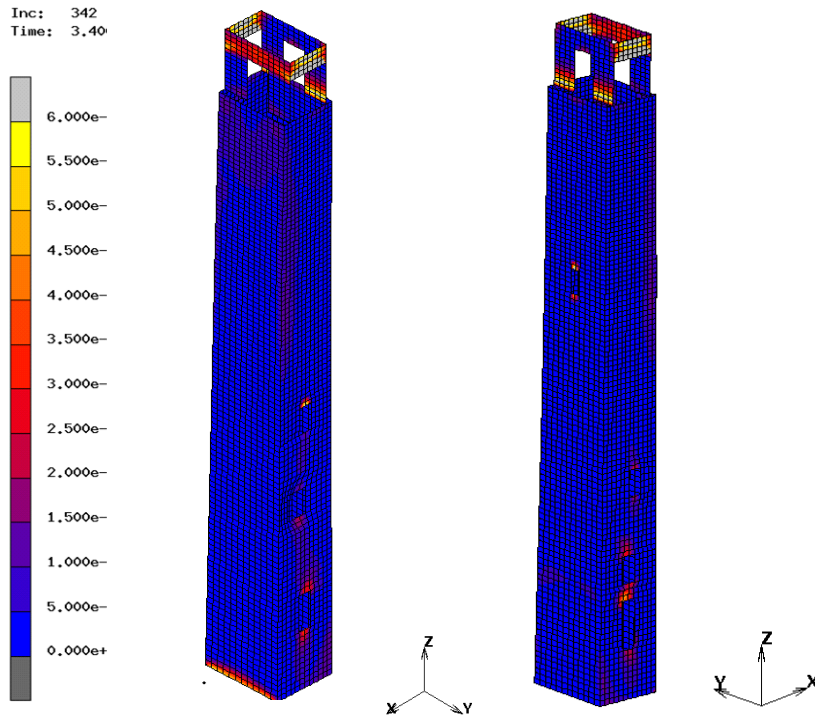


The "Rognosa" tower in San Gimignano: dynamic analysis

Fracture strain E_{zz}^f

At time $t=3,41$ s:

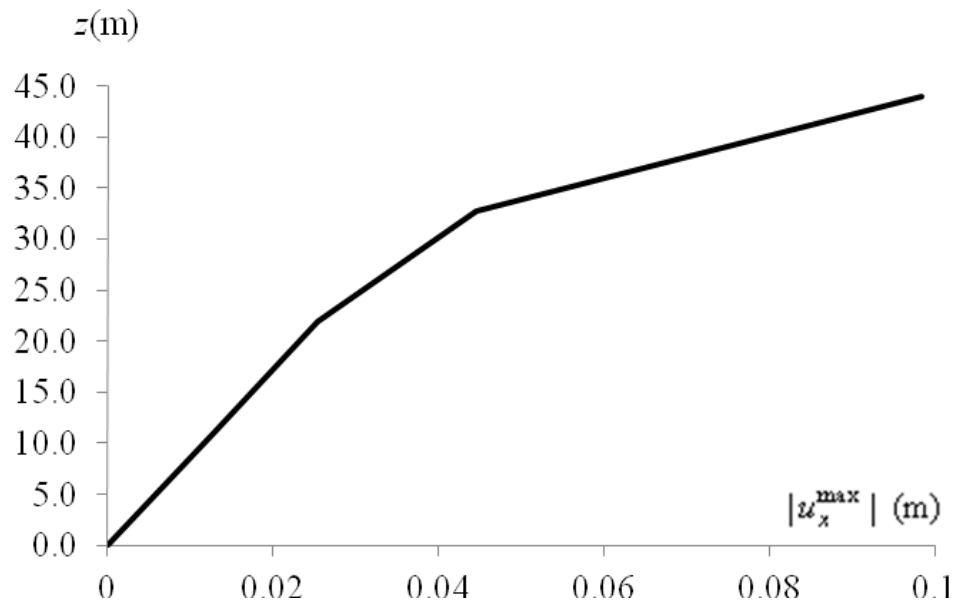
Maximum values reached during the analysis :



The "Rognosa" tower in San Gimignano: dynamic analysis

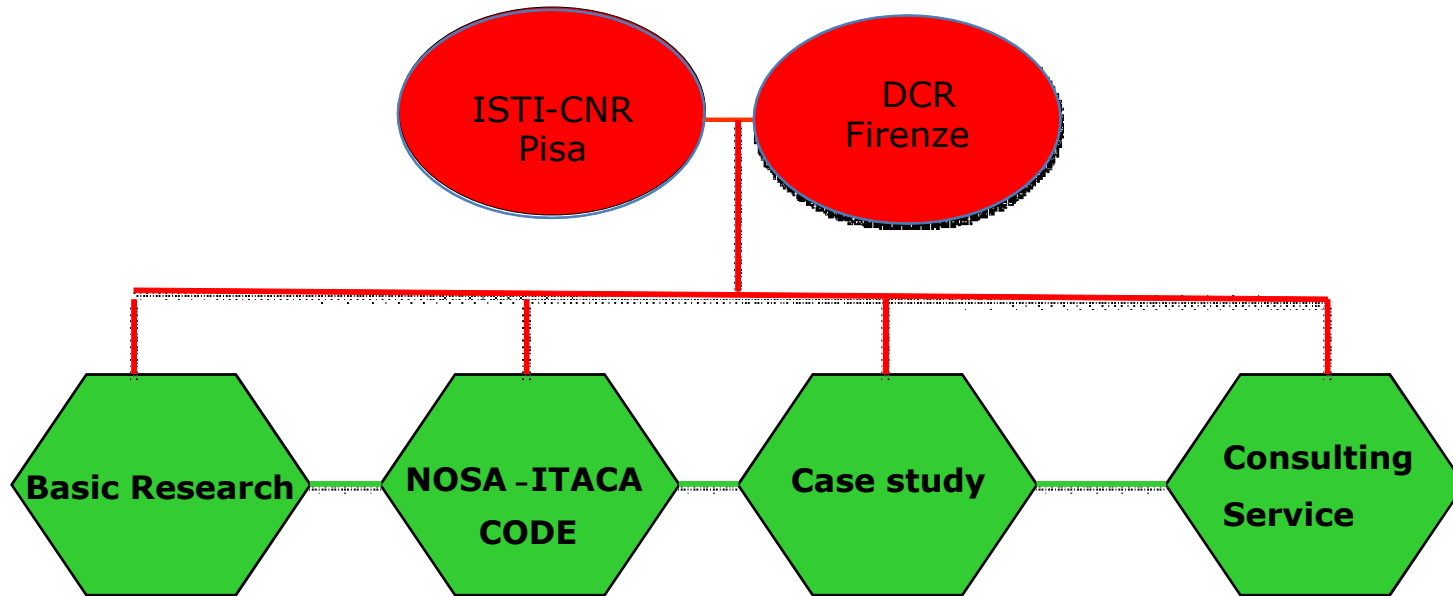
Displacements u_x

Maximum values reached during the analysis:



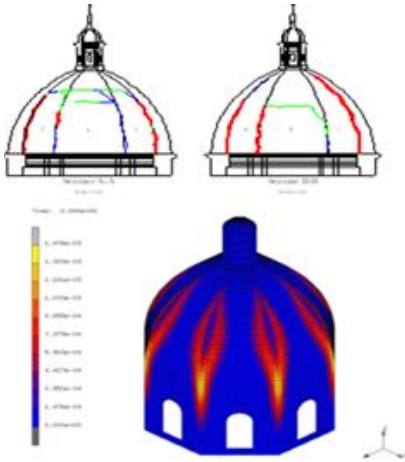
**The NOSA-ITACA project
2011-2013**

funded by the Region of Tuscany (PAR-FAS 2007-2013)

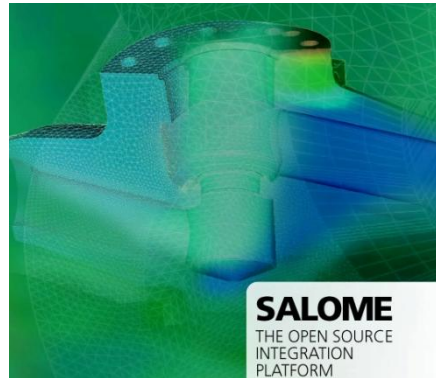


The NOSA-ITACA project

NOSA CODE: f.e.m. nonlinear solver



SALOME: pre-post processor



Case study: "Voltone", Livorno

NOSA-ITACA code

CONSULTING SERVICE

Municipalities
Monuments and Fine Arts Offices
Professional offices

Conclusions

- The NOSA code is a finite element code for static and dynamic nonlinear analyses of masonry structures. The version for static analyses is freely downloadable.
- Masonry is modelled by means of a masonry-like constitutive equation with zero tensile strength and finite or infinite compressive strength.
- A case study has been presented in which the seismic vulnerability of the Rognosa Tower in San Gimignano is assessed by means of a dynamic numerical analysis conducted via NOSA code.
- The NOSA-ITACA project aims to upgrade the NOSA code and disseminate the use of numerical tools in the field of maintenance and restoration of the architectural heritage.